

Table 1: Vertical excitation energies and dominant contributions of the  $S_0$  and  $S_1$  states of fulvene optimized with SA2-CASSCF(6,6)/6-31G\* and MRCI(CAS(6,6))/6-31G\*. For MRCI, the Pople correction is also given (MRCI+Pople).

State	$\Delta E$ (eV)	Configuration	%
SA2-CASSCF(6,6) – $S_0$ optimization			
$S_0$	0.000	$(19a)^2(20a)^2(21a)^2(22a)^0(23a)^0(24a)^0$	77.3
$S_1$	4.110	$(19a)^2(20a)^2(21a)^1(22a)^1(23a)^0(24a)^0$	74.0
		$(19a)^2(20a)^1(21a)^1(22a)^2(23a)^0(24a)^0$	14.1
SA2-CASSCF(6,6) – $S_1$ optimization			
$S_0$	1.446	$(19a)^2(20a)^2(21a)^2(22a)^0(23a)^0(24a)^0$	66.5
		$(19a)^2(20a)^1(21a)^2(22a)^1(23a)^0(24a)^0$	13.8
$S_1$	2.611	$(19a)^2(20a)^2(21a)^1(22a)^1(23a)^0(24a)^0$	72.3
		$(19a)^2(20a)^1(21a)^1(22a)^2(23a)^0(24a)^0$	15.8
SA2-CASSCF(6,6) – MXS optimization - Planar			
$S_0$	2.880	$(19a)^2(20a)^2(21a)^1(22a)^1(23a)^0(24a)^0$	73.0
		$(19a)^2(20a)^1(21a)^1(22a)^2(23a)^0(24a)^0$	15.4
$S_1$	2.880	$(19a)^2(20a)^2(21a)^2(22a)^0(23a)^0(24a)^0$	60.1
		$(19a)^2(20a)^1(21a)^2(22a)^1(23a)^0(24a)^0$	16.8
SA2-CASSCF(6,6) – MXS optimization – nonplanar (fixed 20°)			
$S_0$	2.796	$(19a)^2(20a)^2(21a)^2(22a)^0(23a)^0(24a)^0$	59.8
		$(19a)^2(20a)^1(21a)^2(22a)^1(23a)^0(24a)^0$	17.2
$S_1$	2.796	$(19a)^2(20a)^2(21a)^1(22a)^1(23a)^0(24a)^0$	72.9
		$(19a)^2(20a)^1(21a)^1(22a)^2(23a)^0(24a)^0$	15.4
SA2-CASSCF(6,6) – MXS optimization – nonplanar (fixed 45°)			
$S_0$	2.549	$(19a)^2(20a)^2(21a)^2(22a)^0(23a)^0(24a)^0$	51.1
		$(19a)^2(20a)^1(21a)^2(22a)^1(23a)^0(24a)^0$	17.4
$S_1$	2.549	$(19a)^2(20a)^2(21a)^1(22a)^1(23a)^0(24a)^0$	64.7
		$(19a)^2(20a)^1(21a)^1(22a)^2(23a)^0(24a)^0$	13.6
SA2-CASSCF(6,6) – MXS optimization – nonplanar (63°)			
$S_0$	2.445	$(19a)^2(20a)^2(21a)^1(22a)^1(23a)^0(24a)^0$	73.4
		$(19a)^2(20a)^1(21a)^1(22a)^2(23a)^0(24a)^0$	13.5
$S_1$	2.456	$(19a)^2(20a)^2(21a)^2(22a)^0(23a)^0(24a)^0$	48.1
		$(19a)^2(20a)^1(21a)^2(22a)^1(23a)^0(24a)^0$	28.3
SA2-CASSCF(6,6) – MXS optimization – nonplanar (fixed 70°)			
$S_0$	2.470	$(19a)^2(20a)^2(21a)^1(22a)^1(23a)^0(24a)^0$	79.7
$S_1$	2.470	$(19a)^2(20a)^1(21a)^2(22a)^1(23a)^0(24a)^0$	47.0
		$(19a)^2(20a)^2(21a)^2(22a)^0(23a)^0(24a)^0$	28.3

SA2-CASSCF(6,6) – MXS optimization – nonplanar (fixed 90°)			
S <sub>0</sub>	2.553	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>1</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	87.8
S <sub>1</sub>	2.553	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>1</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	85.5
MRCI – S <sub>0</sub> optimization			
S <sub>0</sub>	0.000/0.000	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>2</sup> (22a) <sup>0</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	69.1
S <sub>1</sub>	3.841/3.633	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>1</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	71.1
MRCI – S <sub>1</sub> optimization			
S <sub>0</sub>	1.235/1.152	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>2</sup> (22a) <sup>0</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	62.3
S <sub>1</sub>	2.609/2.459	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>1</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	67.8
		(19a) <sup>2</sup> (20a) <sup>1</sup> (21a) <sup>1</sup> (22a) <sup>2</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	10.1
MRCI – MXS optimization - Planar			
S <sub>0</sub>	3.022/2.972	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>1</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	62.8
S <sub>1</sub>	3.022/2.860	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>2</sup> (22a) <sup>0</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	52.8
		(19a) <sup>2</sup> (20a) <sup>1</sup> (21a) <sup>2</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	11.9
MRCI – MXS optimization – Nonplanar (fixed 20°)			
S <sub>0</sub>	2.930/2.891	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>1</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	65.9
		(19a) <sup>2</sup> (20a) <sup>1</sup> (21a) <sup>1</sup> (22a) <sup>2</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	10.4
S <sub>1</sub>	2.930/2.769	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>2</sup> (22a) <sup>0</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	55.4
		(19a) <sup>2</sup> (20a) <sup>1</sup> (21a) <sup>2</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	12.8
MRCI – MXS optimization – Nonplanar (fixed 45°)			
S <sub>0</sub>	2.649/2.584	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>1</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	40.4
		(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>2</sup> (22a) <sup>0</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	21.3
S <sub>1</sub>	2.649/2.559	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>2</sup> (22a) <sup>0</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	33.0
		(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>1</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	26.1
MRCI – MXS optimization – nonplanar (65.1°)			
S <sub>0</sub>	2.519/2.521	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>1</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	66.9
S <sub>1</sub>	2.519/2.423	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>2</sup> (22a) <sup>0</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	45.1
		(19a) <sup>2</sup> (20a) <sup>1</sup> (21a) <sup>2</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	23.7
MRCI – MXS optimization – Nonplanar (fixed 70°)			
S <sub>0</sub>	2.527/2.446	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>2</sup> (22a) <sup>0</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	39.3
		(19a) <sup>2</sup> (20a) <sup>1</sup> (21a) <sup>2</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	29.2
S <sub>1</sub>	2.527/2.534	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>1</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	67.7
MRCI – MXS optimization – Nonplanar (fixed 90°)			
S <sub>0</sub>	2.618/2.628	(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>1</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	63.2
		(19a) <sup>2</sup> (20a) <sup>1</sup> (21a) <sup>2</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	13.0
S <sub>1</sub>	2.618/2.595	(19a) <sup>2</sup> (20a) <sup>1</sup> (21a) <sup>2</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	62.9
		(19a) <sup>2</sup> (20a) <sup>2</sup> (21a) <sup>1</sup> (22a) <sup>1</sup> (23a) <sup>0</sup> (24a) <sup>0</sup>	13.1

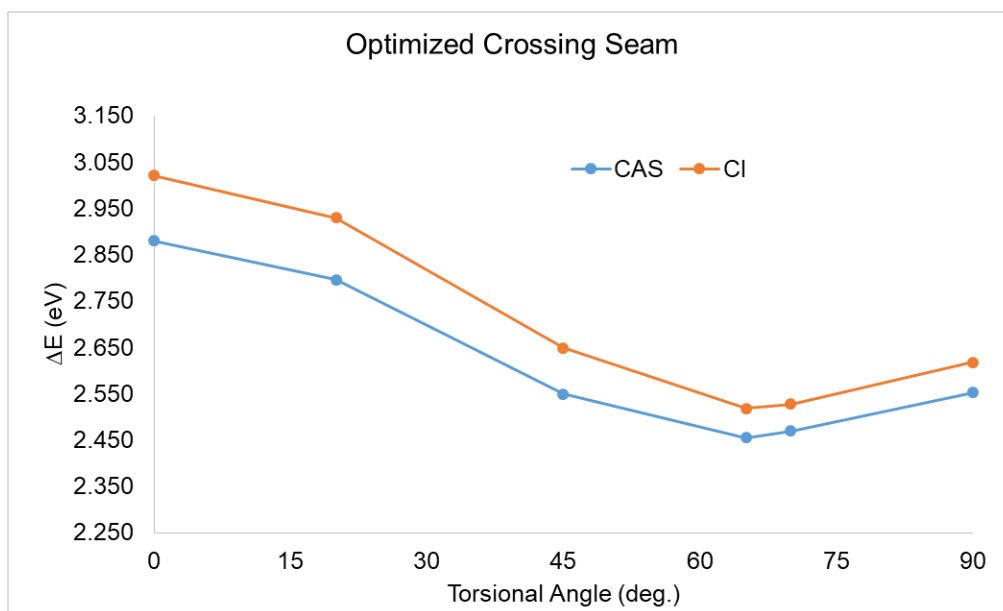


Figure 1: Relative energy of the optimized crossing seam between the  $S_0$  and  $S_1$  states using the SA2-CASSCF(6,6)/6-31G\* and MRCI(CAS(6,6))/6-31G\* methods. Energies relative to the optimized  $S_0$  ground state in each method.

Table 2: Total energies in Hartree of fulvene

	S <sub>0</sub>	S <sub>1</sub>
SA2-CASSCF(6,6)-S <sub>0</sub> opt	-230.72231	-230.57127
SA2-CASSCF(6,6)-S <sub>1</sub> opt	-230.66916	-230.62635
SA2-CASSCF(6,6)-MXS-planar	-230.61647	-230.61647
SA2-CASSCF(6,6)-MXS-nonplanar (20°)	-230.61957	-230.61955
SA2-CASSCF(6,6)-MXS-nonplanar (45°)	-230.62862	-230.62862
SA2-CASSCF(6,6)-MXS-nonplanar (63°)	-230.63208	-230.63206
SA2-CASSCF(6,6)-MXS-nonplanar (70°)	-230.63154	-230.63154
SA2-CASSCF(6,6)-MXS-nonplanar (90°)	-230.62850	-230.62850
MRCI-S <sub>0</sub> opt	-231.33320	-231.19206
MRCI+Q-S <sub>0</sub> opt	-231.46471	-231.33121
MRCI-S <sub>1</sub> opt	-231.28780	-231.23732
MRCI+Q-S <sub>1</sub> opt	-231.42239	-231.37102
MRCI-MXS-planar	-231.22216	-231.22216
MRCI+Q-MXS-planar	-231.35550	-231.35960
MRCI-MXS-nonplanar (20°)	-231.22553	-231.22553
MRCI+Q-MXS-nonplanar (20°)	-231.35848	-231.36297
MRCI-MXS-nonplanar (45°)	-231.23585	-231.23585
MRCI+Q-MXS-nonplanar (45°)	-231.36976	-231.37068
MRCI-MXS-nonplanar (65.1°)	-231.24064	-231.24064
MRCI+Q-MXS-nonplanar (65.1°)	-231.37206	-231.37566
MRCI-MXS-nonplanar (70°)	-231.24033	-231.24033
MRCI+Q-MXS-nonplanar (70°)	-231.37480	-231.37157
MRCI-MXS-nonplanar (90°)	-231.23698	-231.23698
MRCI+Q-MXS-nonplanar (90°)	-231.36814	-231.36934

Table 3: Oscillator strength of the S<sub>0</sub> to S<sub>1</sub> transition of fulvene optimized with SA2-CASSCF(6,6)/6-31G\* and MRCI(CAS(6,6))/6-31G\*.

Method	<i>f</i>
SA2-CASSCF(6,6) – S <sub>0</sub> optimization	0.00
SA2-CASSCF(6,6) – S <sub>1</sub> optimization	0.00
MRCI – S <sub>0</sub> optimization	0.01
MRCI – S <sub>1</sub> optimization	0.00

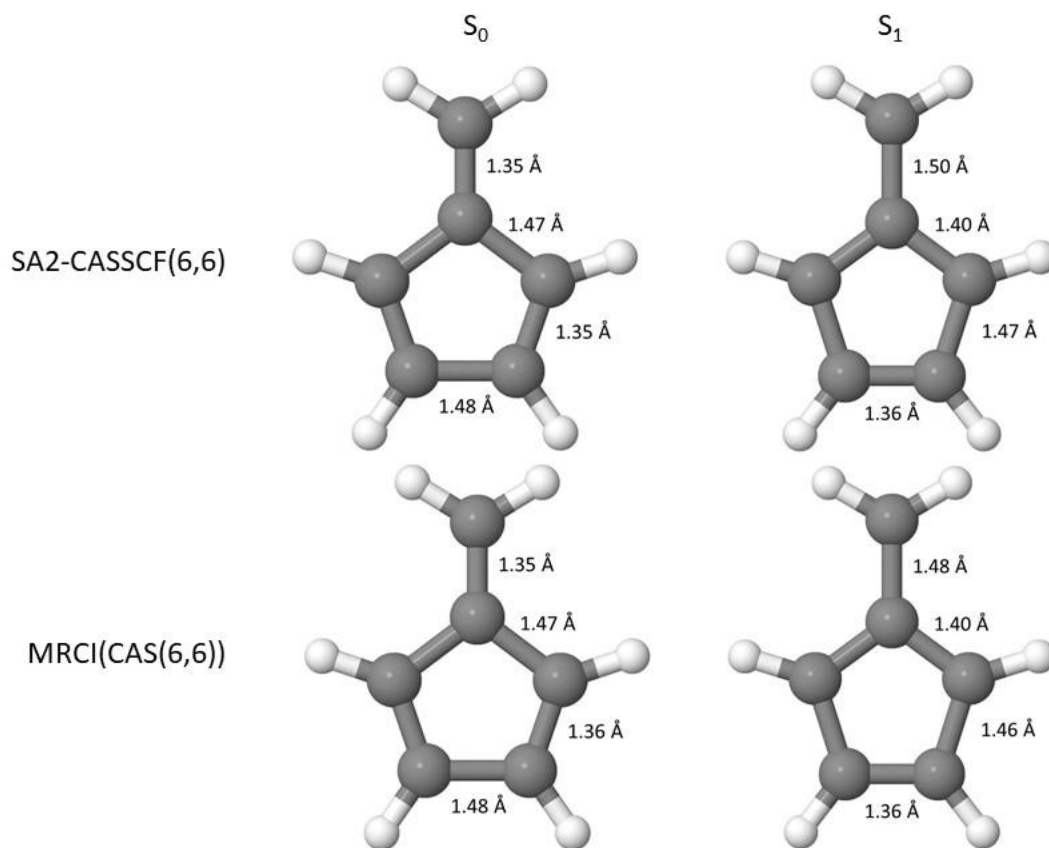


Figure 2: Bond distances of the  $S_0$  to  $S_1$  states optimized with SA2-CASSCF(6,6)/6-31G\* and MRCI(CAS(6,6))/6-31G\*.

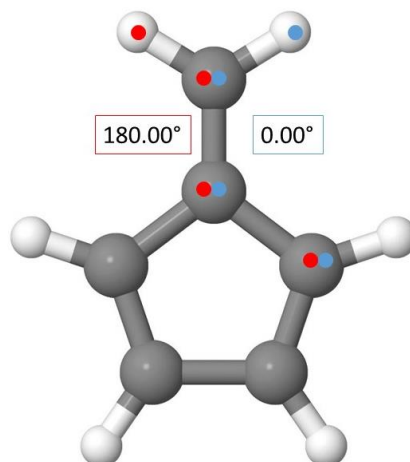


Figure 3: Torsional angles of the  $S_0$  to  $S_1$  states optimized with SA2-CASSCF(6,6)/6-31G\* and MRCI(CAS(6,6))/6-31G\*. The molecule is planar, so there is no variation. Torsional angles, blue and red, are designated with colored dots.

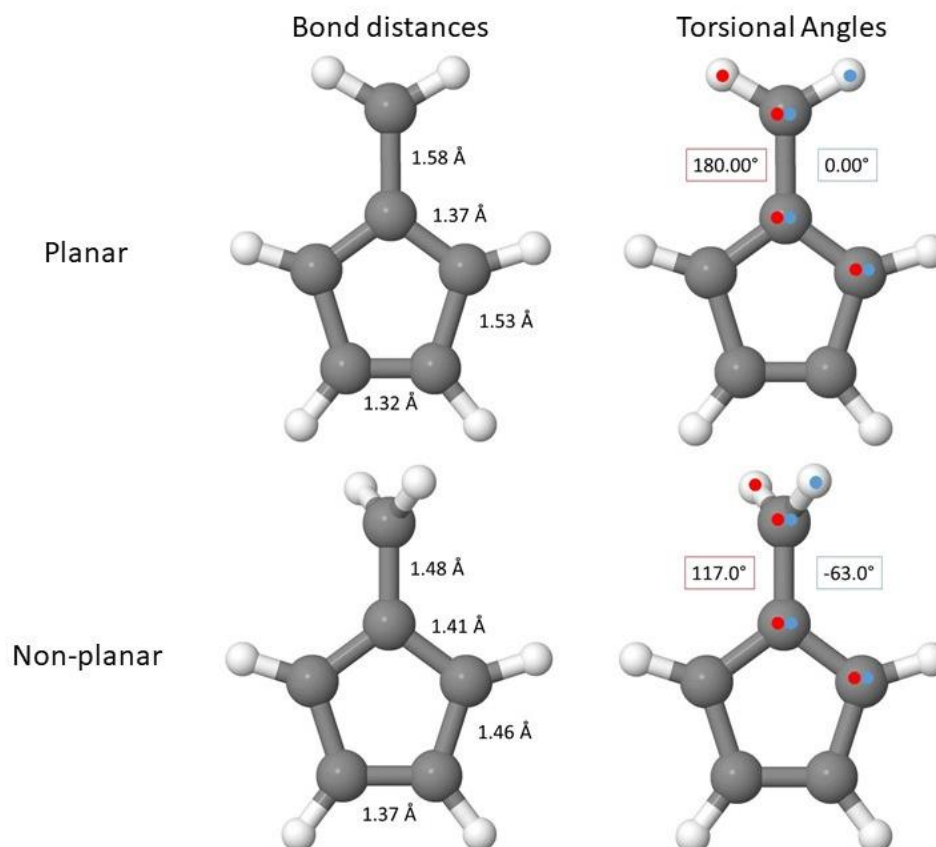
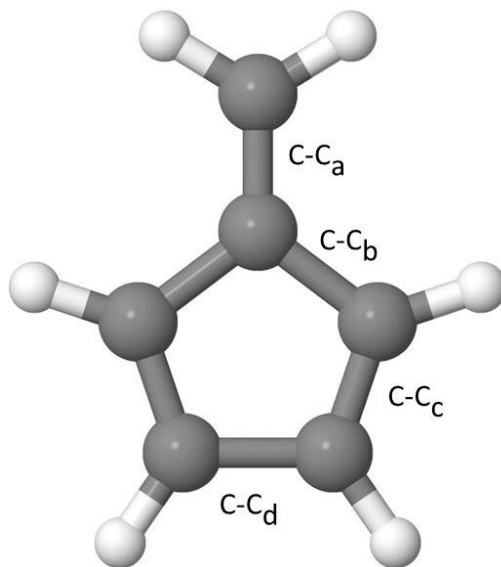


Figure 4: Bond distances and torsional angles of the optimized crossing seam between the  $S_0$  to  $S_1$  states optimized with SA2-CASSCF(6,6)/6-31G\*. Torsional angles, blue and red, are designated with colored dots.

Table 4: C-C bond distances for each fixed torsional angle about the CH<sub>2</sub> group using the SA2-CASSCF(6,6)/6-31G\* and MRCI(CAS(6,6))/6-31G\* methods.



Torsional Angle	C-C <sub>a</sub>	C-C <sub>b</sub>	C-C <sub>c</sub>	C-C <sub>d</sub>
SA2-CASSCF(6,6)				
20.0°	1.56	1.37	1.52	1.32
45.0°	1.51	1.39	1.49	1.34
63.0°	1.48	1.41	1.46	1.37
70.0°	1.47	1.41	1.44	1.38
90.0°	1.48	1.42	1.42	1.41
MRCI				
20.0°	1.56	1.37	1.53	1.32
45.0°	1.51	1.38	1.50	1.33
65.1°	1.47	1.40	1.46	1.37
70.0°	1.47	1.41	1.45	1.38
90.0°	1.47	1.42	1.42	1.41

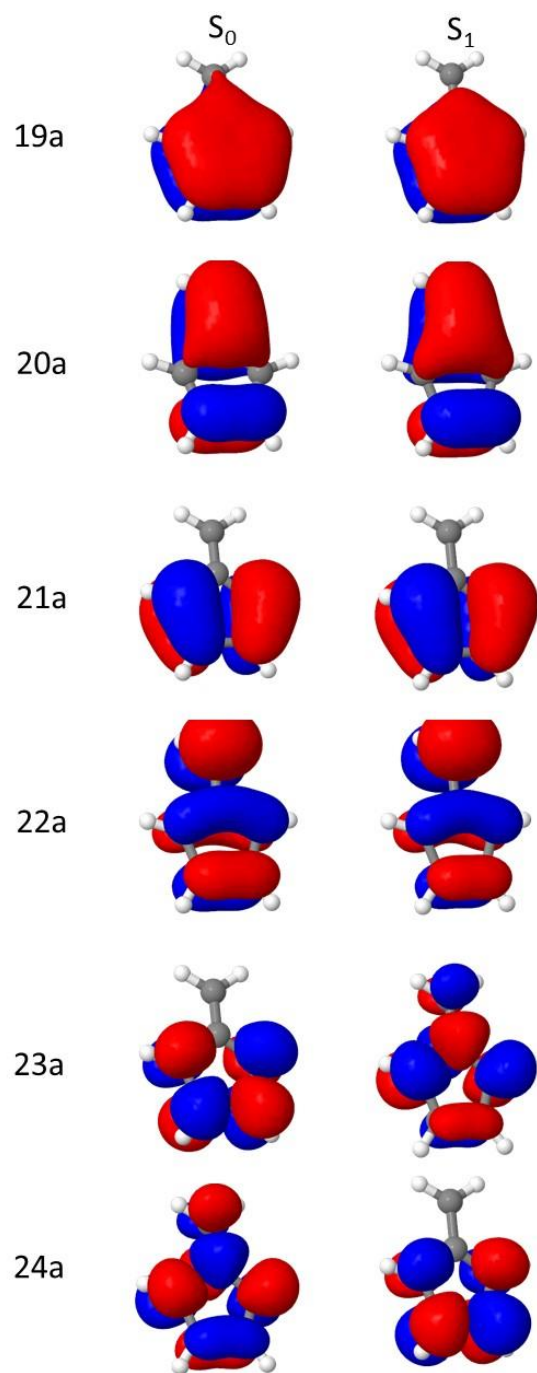


Figure 5: Optimized active orbitals for the  $S_0$  and  $S_1$  states, respectively, optimized with SA2-CASSCF(6,6)/6-31G\*.



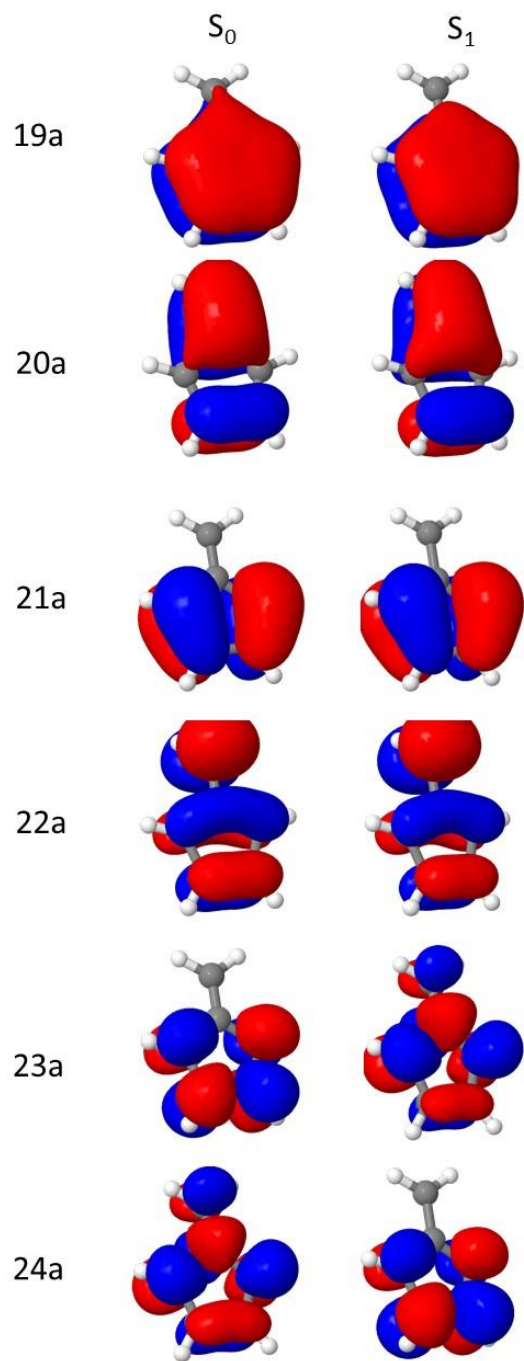


Figure 6: Optimized active orbitals for the  $S_0$  and  $S_1$  states, respectively, optimized with MRCI(CAS(6,6))/6-31G\*.

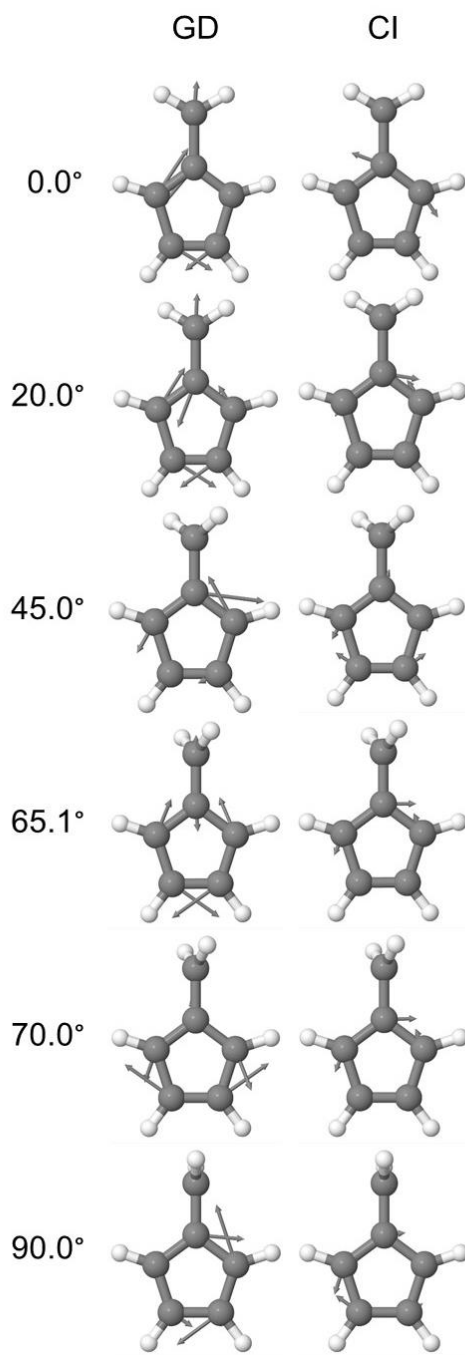


Figure 7: Plots of the GD and CI vectors of fulvene at the optimized crossing seam for several torsional angles going to the -CH<sub>2</sub> group. The MRCI(CAS(6,6))/6-31G\* was utilized. The lowest energy structure at the crossing seam corresponds to 65.1°.

